



Maximizing Production After Stimulation in Tight Gas Reservoirs

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Can Modeling Help Design Fracture Treatments?

- Fracture geometry prediction is improving
 - computing of in-situ stresses
 - Must be calibrated to field measurements
 - measuring and modeling rheology
 - Sensitive to environmental variables
 - predicting prop transport and post-closure movement
 - Modeling and predicting screenouts
 - Requires pre-frac injection and careful diagnostics
 - fracture containment mechanisms other than stress contrast
 - Can be calibrated locally based on observations



Placing Problem Jobs

- Near-well restrictions and high injection pressures
 - Step-rate tests to separate perf restrictions from “tortuosity”
- Rapid near-well screenouts
 - Fluid stability (?)
 - Fissure PDL and proppant holdup
- Increasing pressure to limits during the pad
 - Reservoir conditioning at low rate



Designing for Expected Conductivity

- Include major damage effects
 - non-Darcy and multiphase flow effects
 - non-uniform stress, prop crushing and traditional conductivity
 - channelized flow, saturation distributions and gravity override
 - fluid stability, breaker effectiveness, cleanup, flowback and post-treatment
- Integrate reservoir deliverability and pack damage to estimate effective producing frac length



Post-Job Analysis

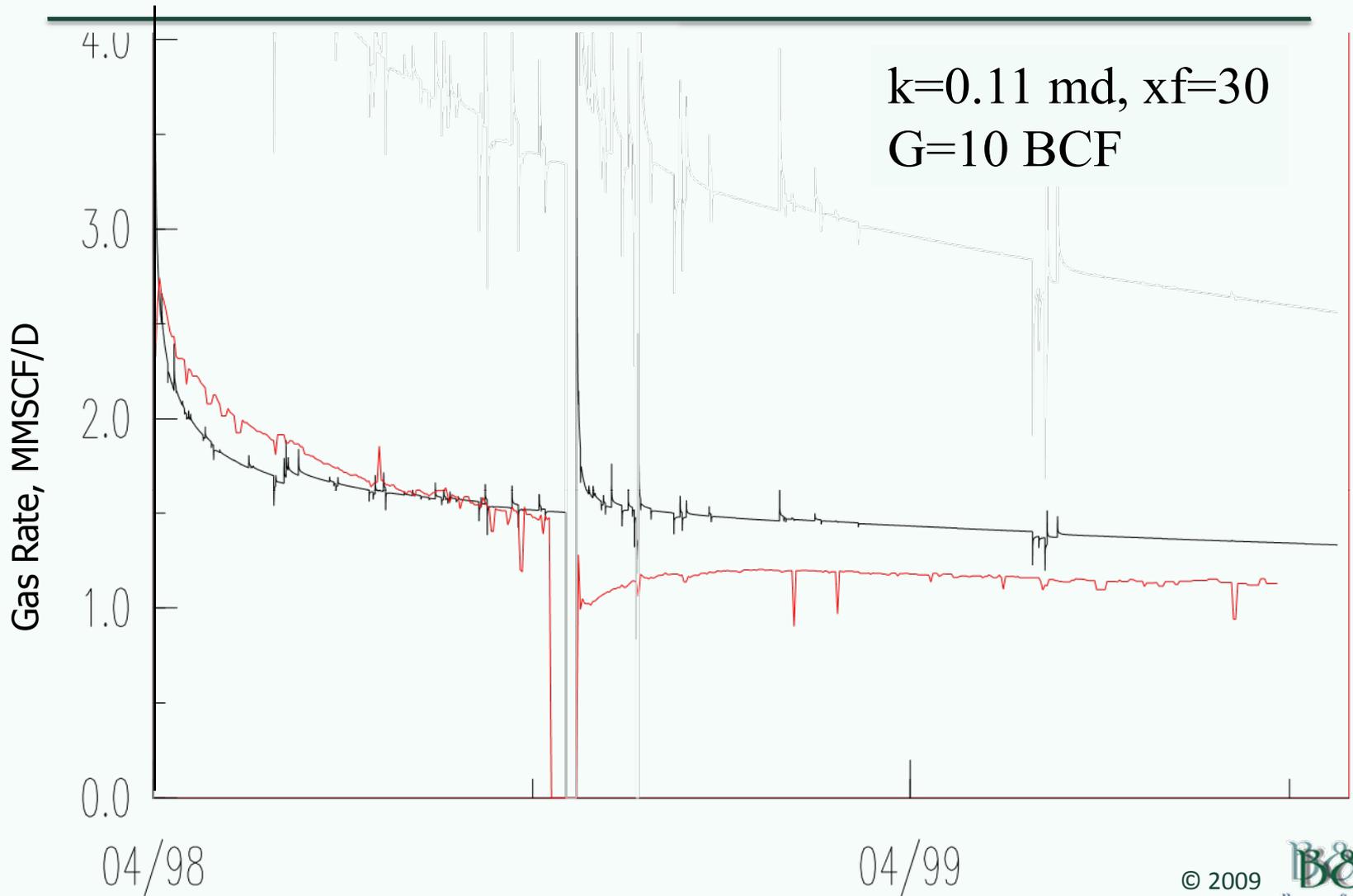
- We must know what was achieved to improve the design
- Production analysis is still the best tool around
 - How the frac behaves during production pays for the treatment
- Collect the data!
- Do the work, or the design effort was wasted



Effect of Liquid Loading on Gas Well Production

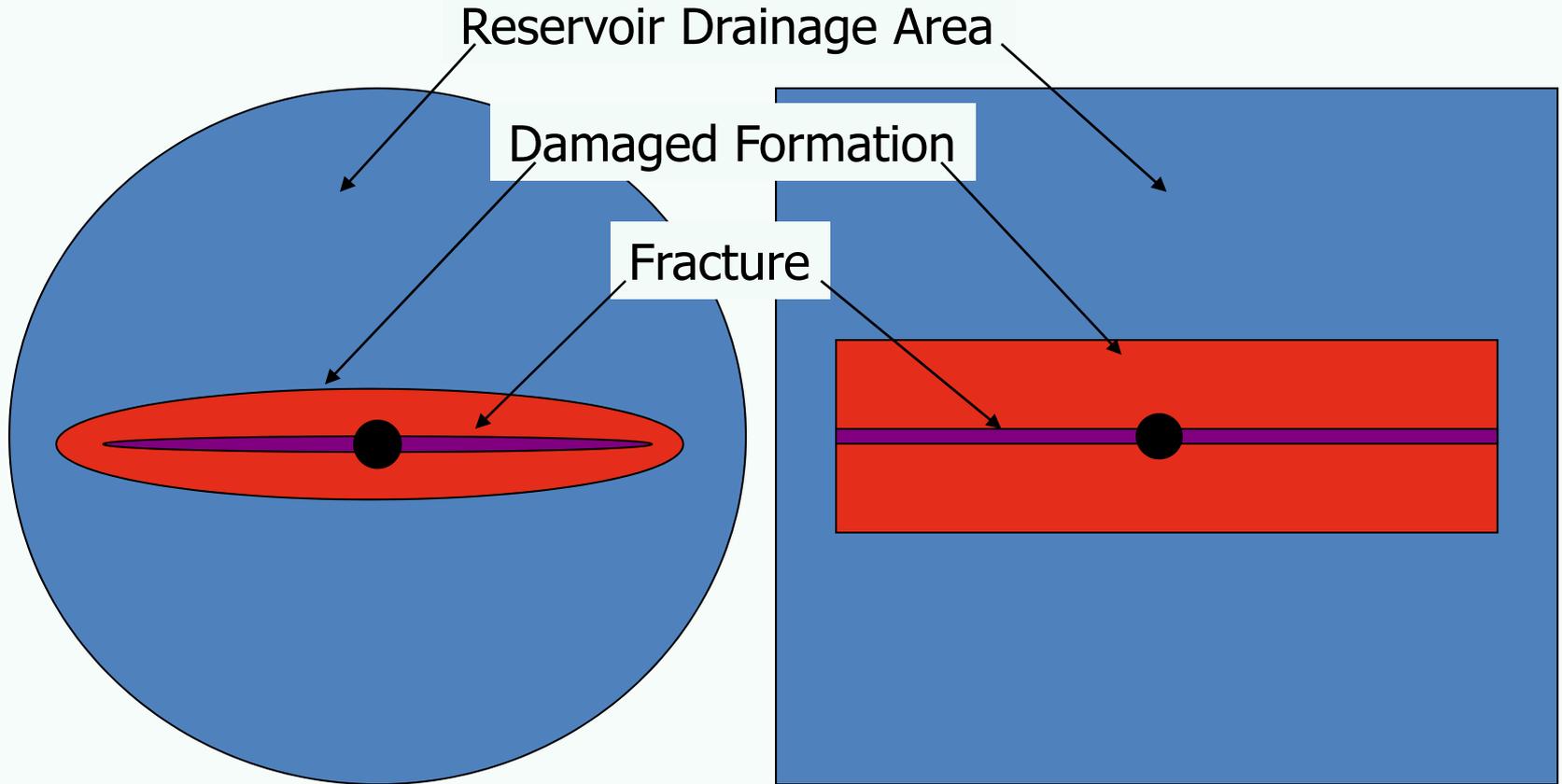
- Impact of short-term well killing or shut-ins
 - Application of snubbing instead of killing
- Capillary pressure and phase trapping
- Proper and improper use of surfactants

Fractured Well Performance Showing Effects of a Short Shut-In





Fracture Face Skin Damage

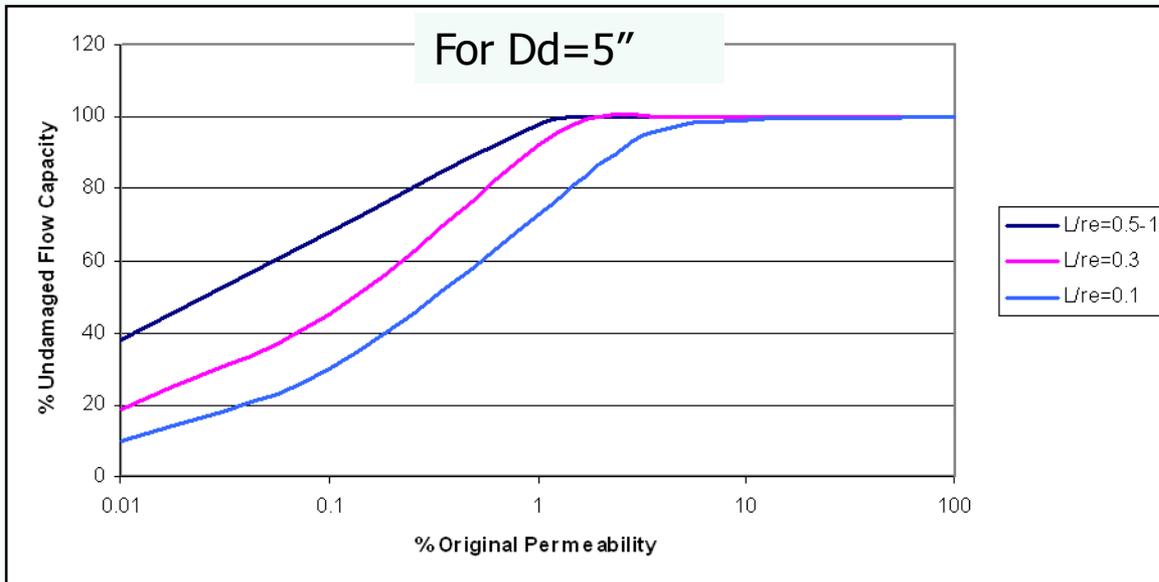
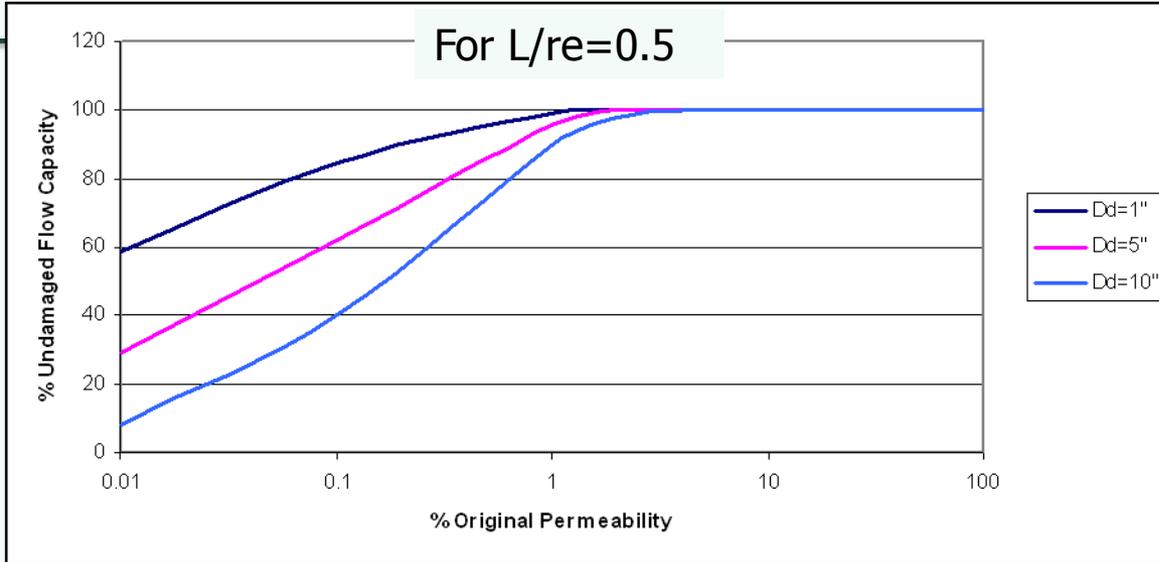


Pratts Analytical Model

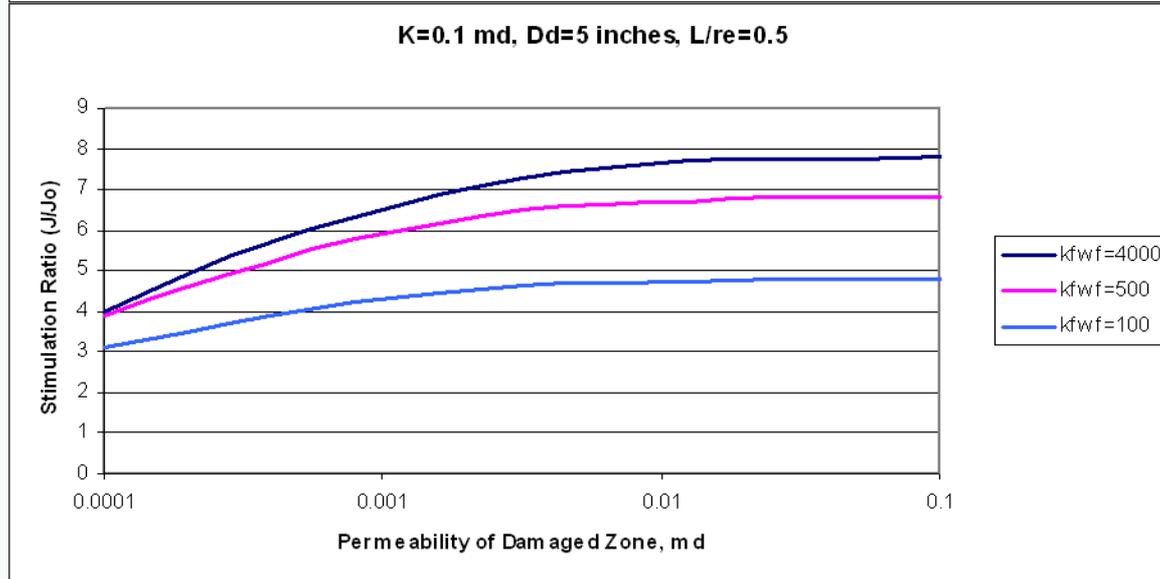
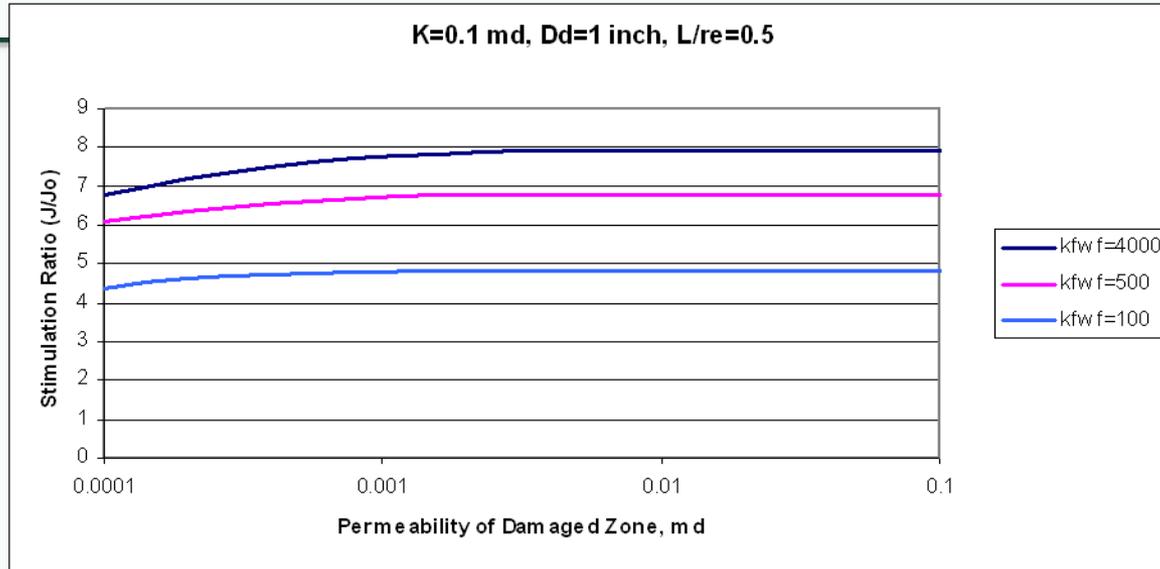
Holditch Numerical Model



Pratts Results Paraphrased



Holditch Results for Face Damage





Another Look at Face Damage

- Pratts and Holditch both assumed that the entire fracture surface area was open to flow
- Permeability is reduced at the face, but remains non-zero
- The large surface area and very low velocity (low pressure gradient) makes perm damage tolerable
- If the fracture face area is diminished (by capillary blockage), it cannot contribute to flow (perm=zero) and their conclusions are invalid
- Inflow capacity is reduced by the ratio of open face area
- Pressure gradients and damage effects are much more severe where flow can occur

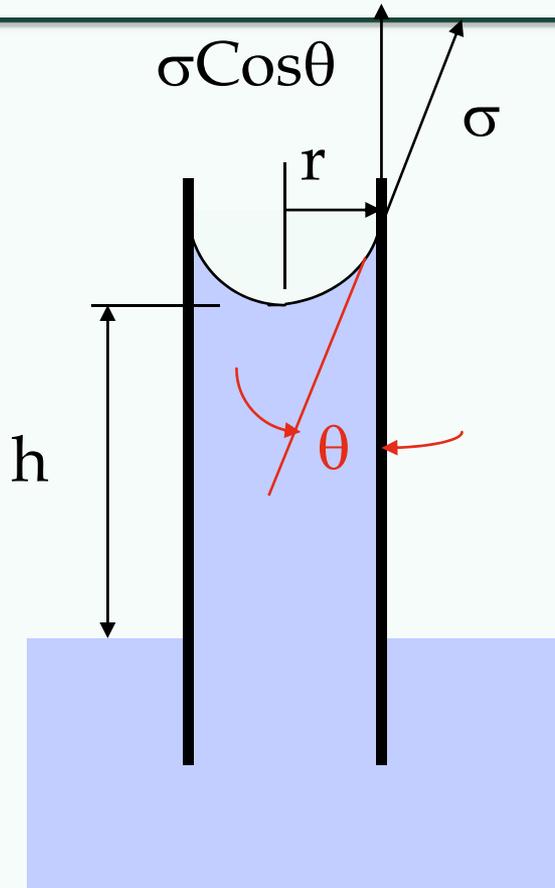


Capillary Pressure

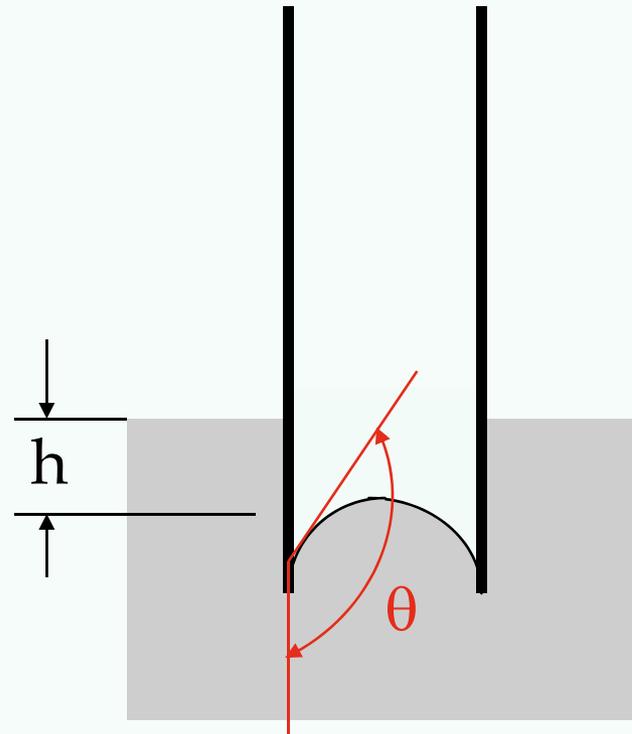
- The difference between the pressures of two or more immiscible phases contained in a restricted cavity is P_c
- Capillary pressure is related to pore size, size distribution, and wettability
- Saturation distribution within a porous medium is controlled by capillary pressure.



Capillary Effects in Circular Tubes



Capillary Rise of a Wetting Phase



Capillary Depression of a Non-Wetting Phase



Capillary Pressure Equations

At equilibrium (no movement of interface):

Force Up = Force Down

$$\text{Force Up} = 2\pi r\sigma\text{Cos}\theta$$

$$\text{Force Down} = \pi r^2 \Delta\rho g h$$

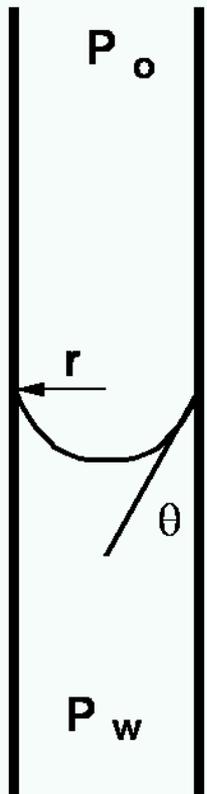
Capillary Pressure is defined as Force per Unit Area (πr^2):

$$P_c = \frac{2\pi r\sigma\text{Cos}\theta}{\pi r^2} = \frac{2\sigma\text{Cos}\theta}{r} \text{ and}$$

$$P_c = \frac{\pi r^2 \Delta\rho h g / g_c}{\pi r^2} = \Delta\rho h \frac{g}{g_c}$$

$$\text{So: } P_c = \frac{2\sigma\text{Cos}\theta}{r} = \Delta\rho \frac{g}{g_c} h$$

Capillary Pressure and Frontal Advance Rate



$$P_c = P_o - P_w$$
$$= \frac{2\sigma \cos \theta}{r}$$

$$V = \frac{r^2 \Delta P}{4\mu \Delta L}$$

Must exceed the threshold capillary pressure to get the interface to move.

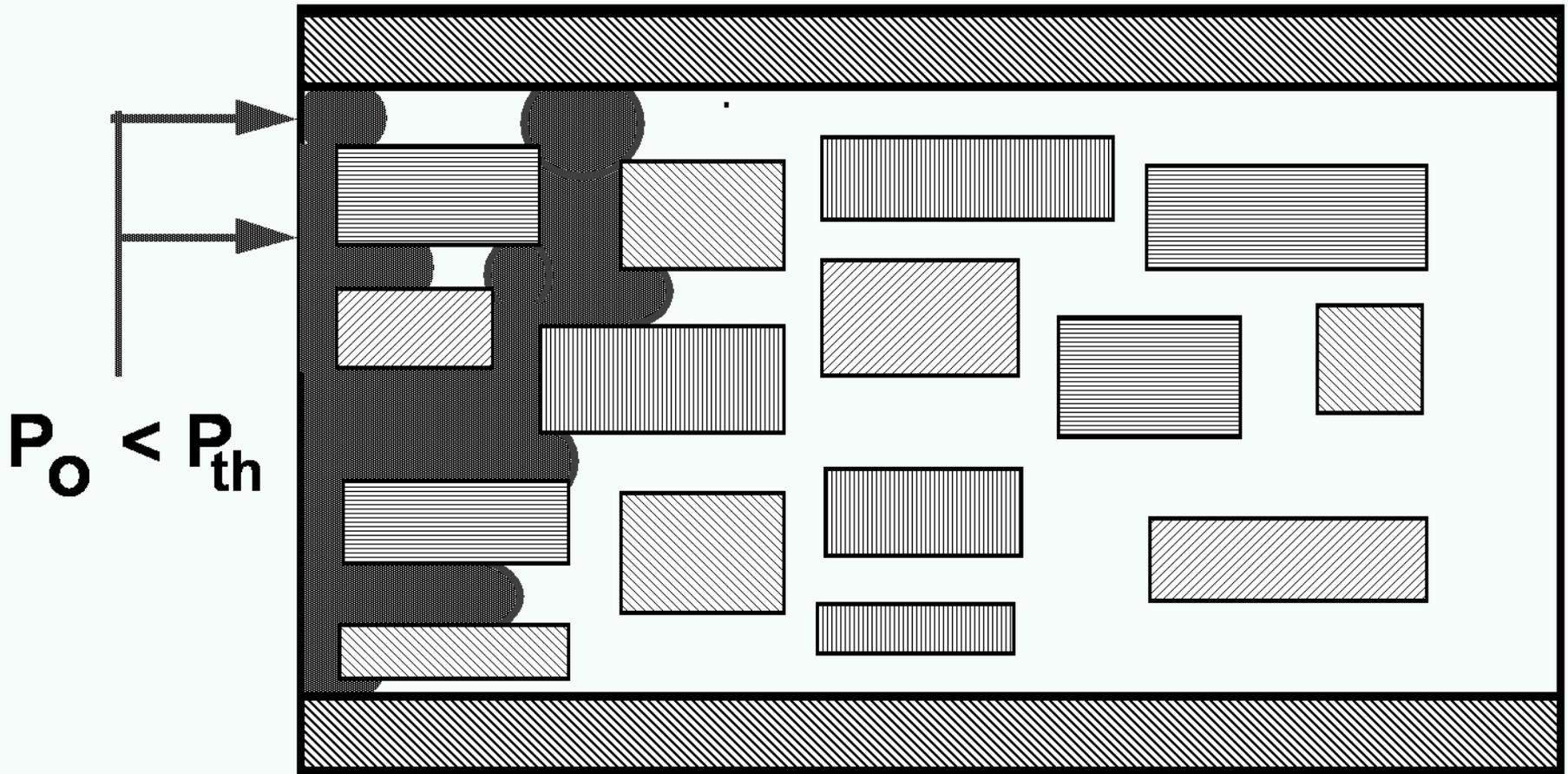
Any pressure differential below the threshold just distends the meniscus.

Once the interface moves, the frontal advance rate is controlled by viscous flow.

Note that both threshold pressure and velocity favor flow in large pores for any potential-driven flow.



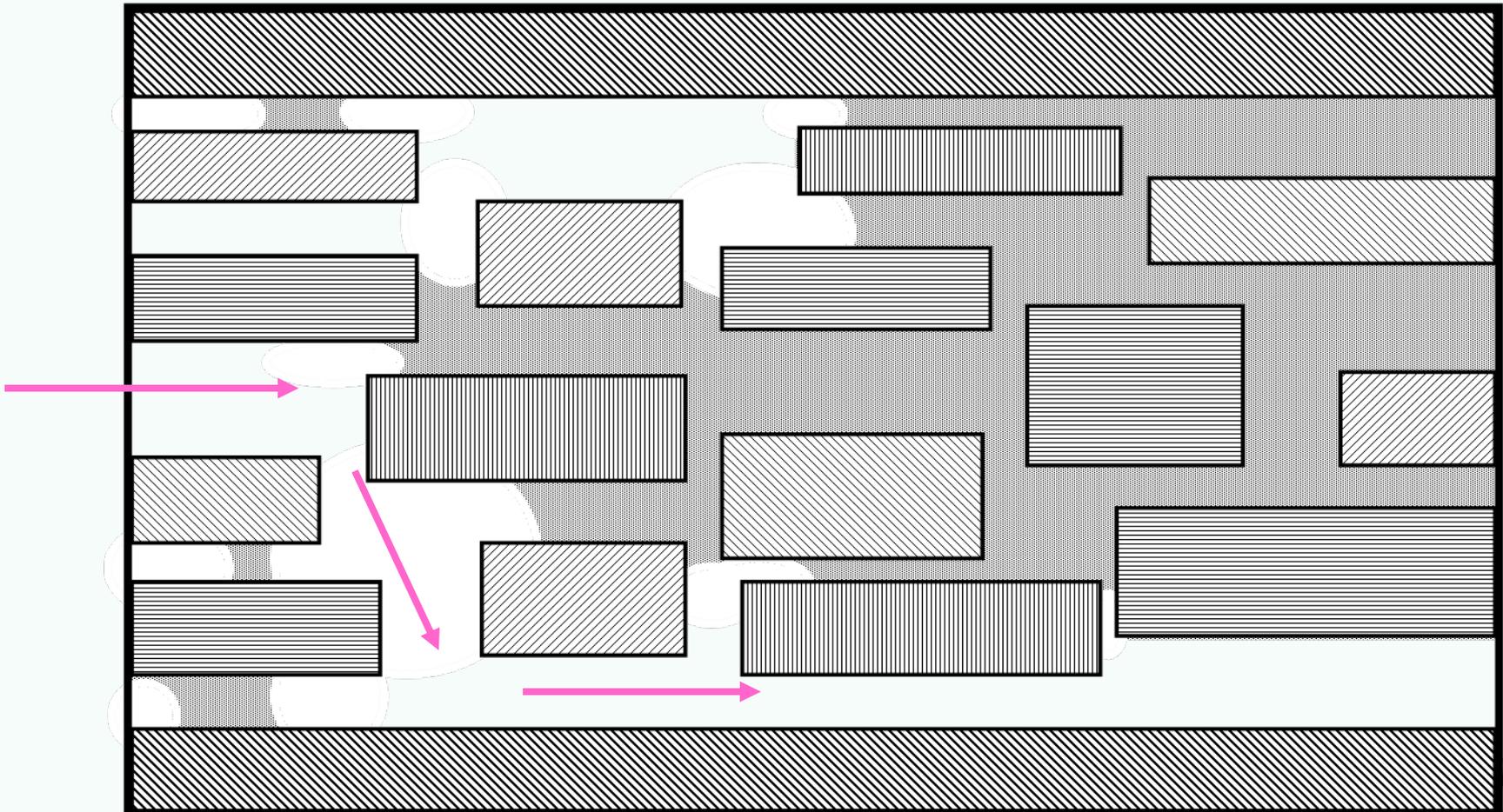
Capillary Pressure restricts fluid entry by pore size



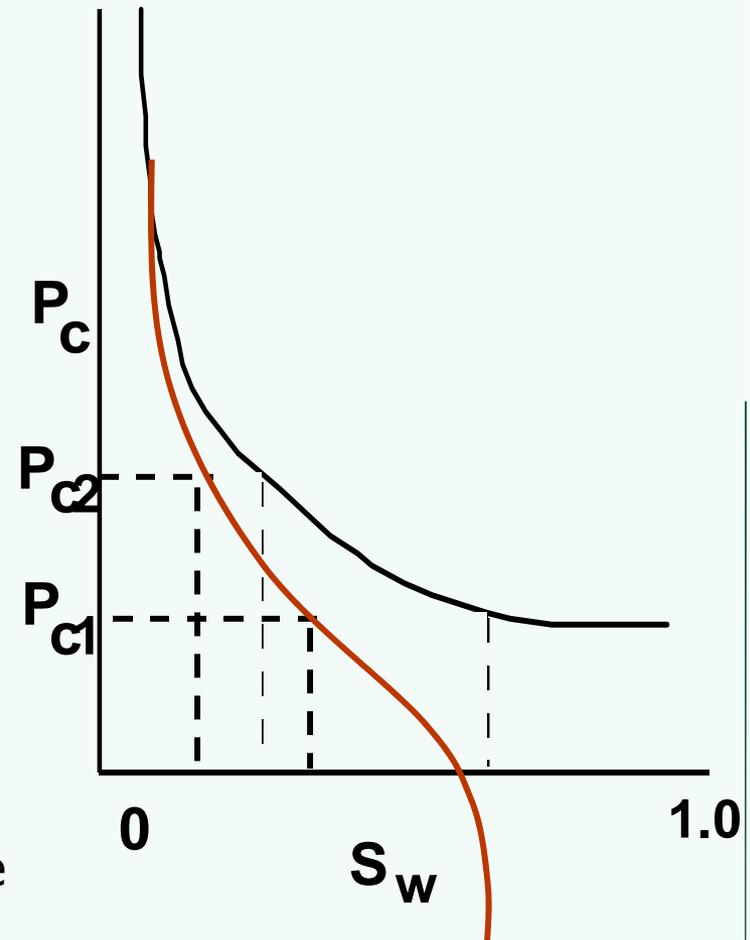
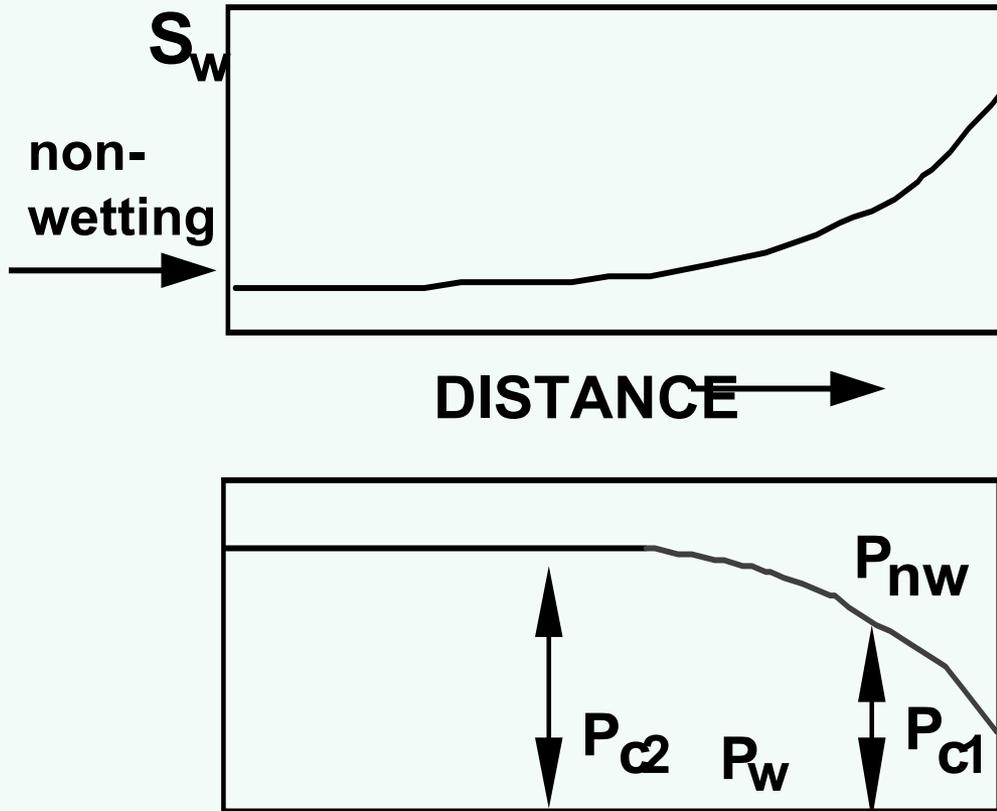


Gas Evolution is Different From Gas Injection

Injected gas can only enter pores based on threshold entry pressure. Gas flow is restricted to few pore channels.



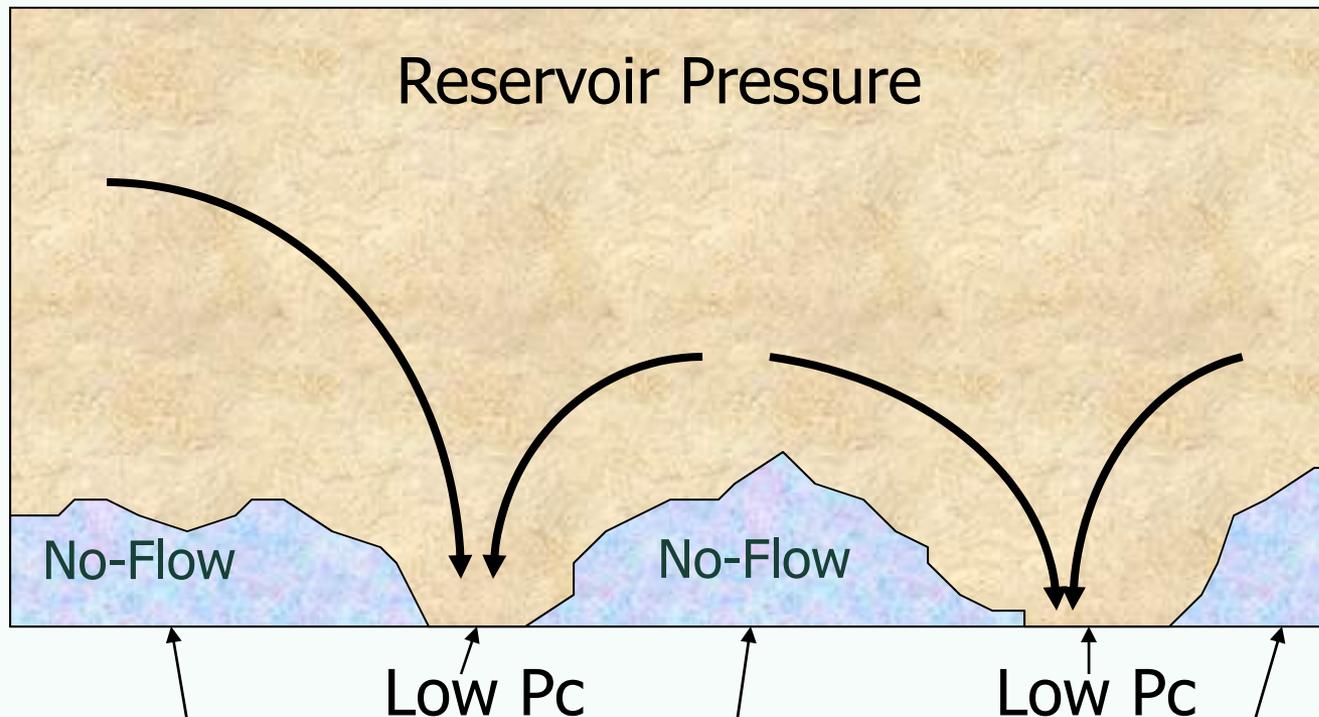
What causes capillary saturation blockage after breakthrough?



Outside the reservoir the capillary pressure approaches zero as radius of curvature of the gas bubble or oil droplet increases.

Capillary Phase Trapping: A Potentially Serious Damage Mechanism

Capillary blocking causes loss of fracture face area



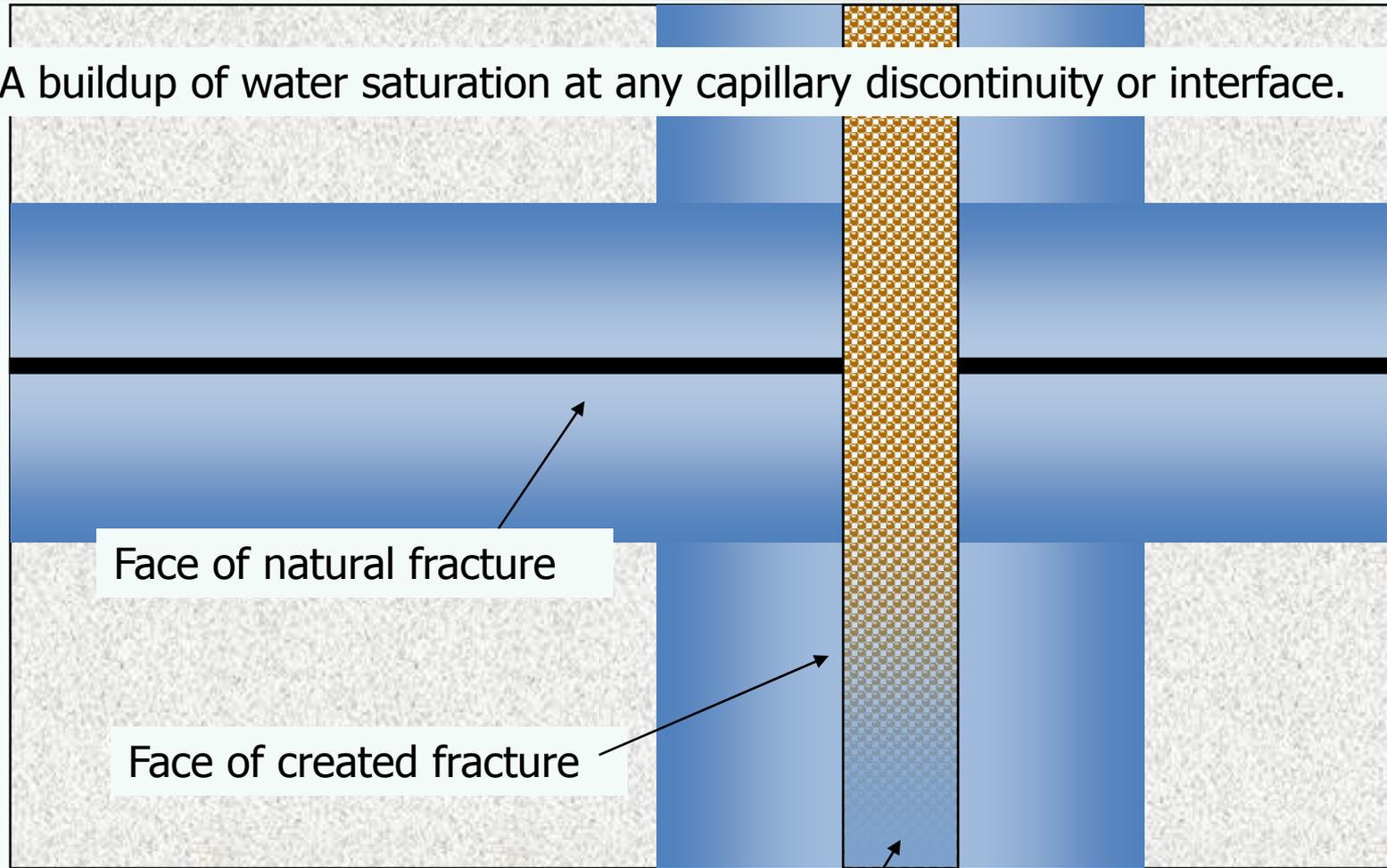
Areas of low porosity, high capillary pressure

Fracture or wellbore pressure under drawdown



Capillary Face Discontinuities or “Capillary End-Effect”

A buildup of water saturation at any capillary discontinuity or interface.



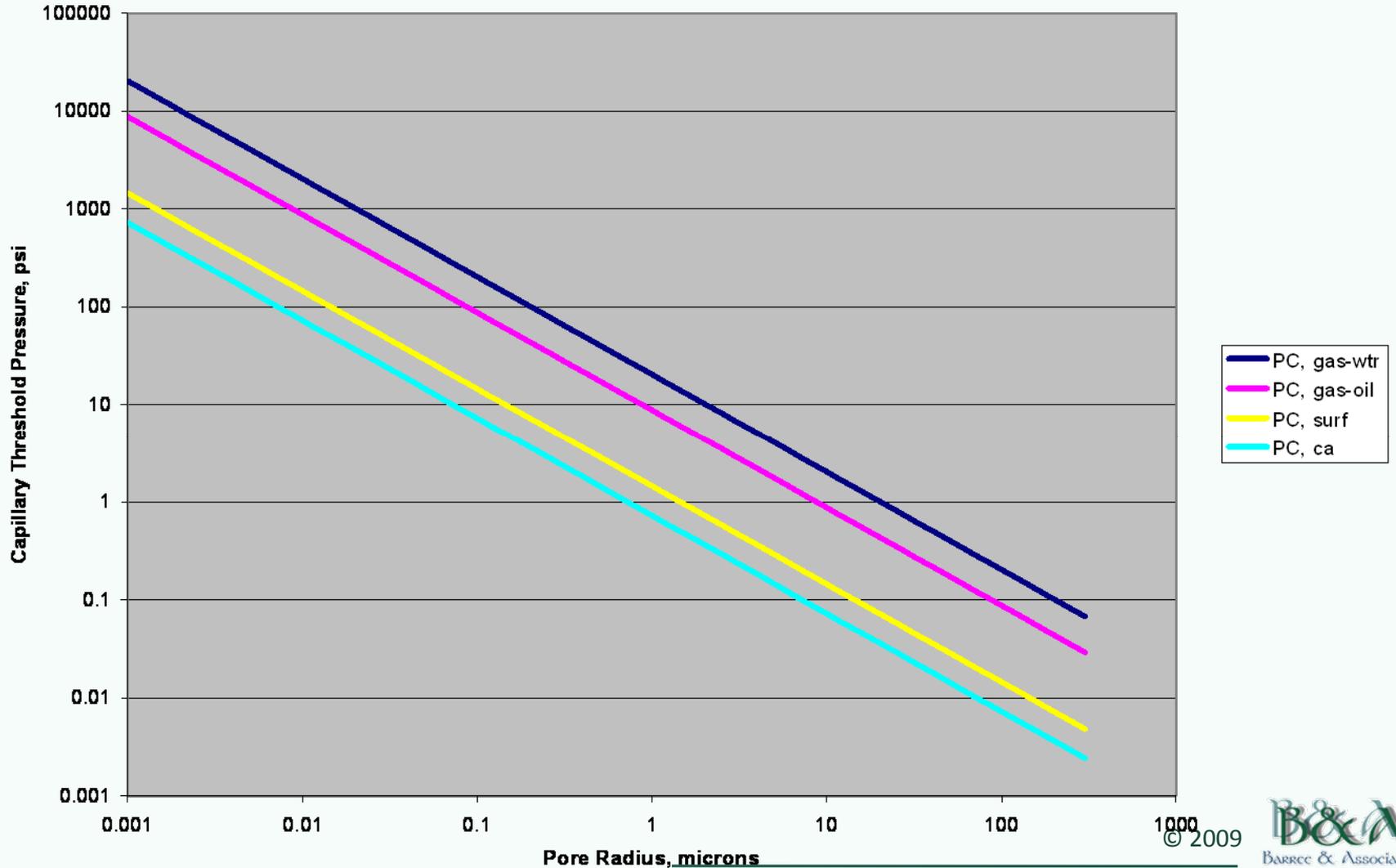
Face of natural fracture

Face of created fracture

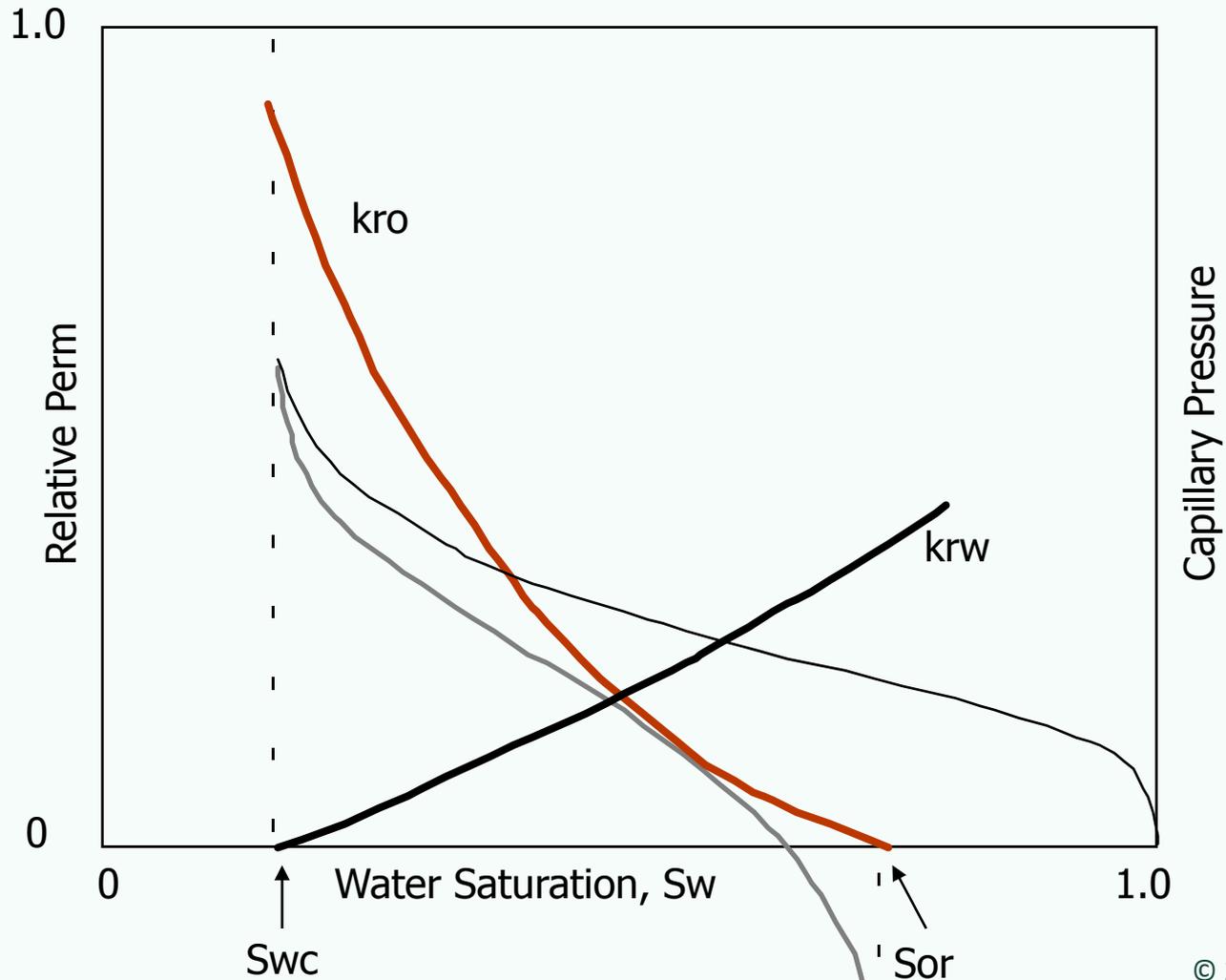
Proppant pack to open perf or wellbore

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Capillary Threshold Pressure for Various Fluid Systems

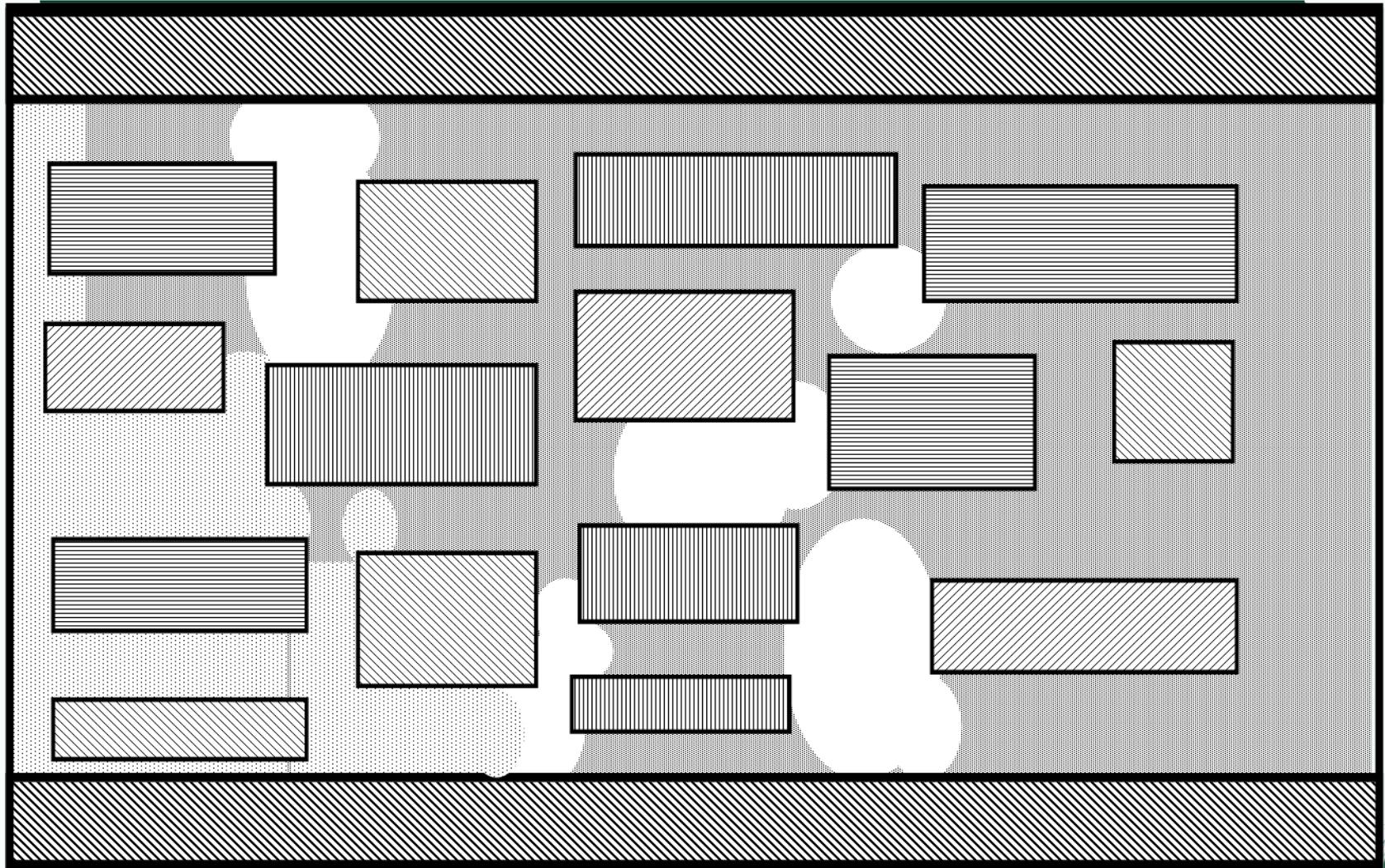


Drainage and Imbibition Residual Saturations at Capillary Equilibrium

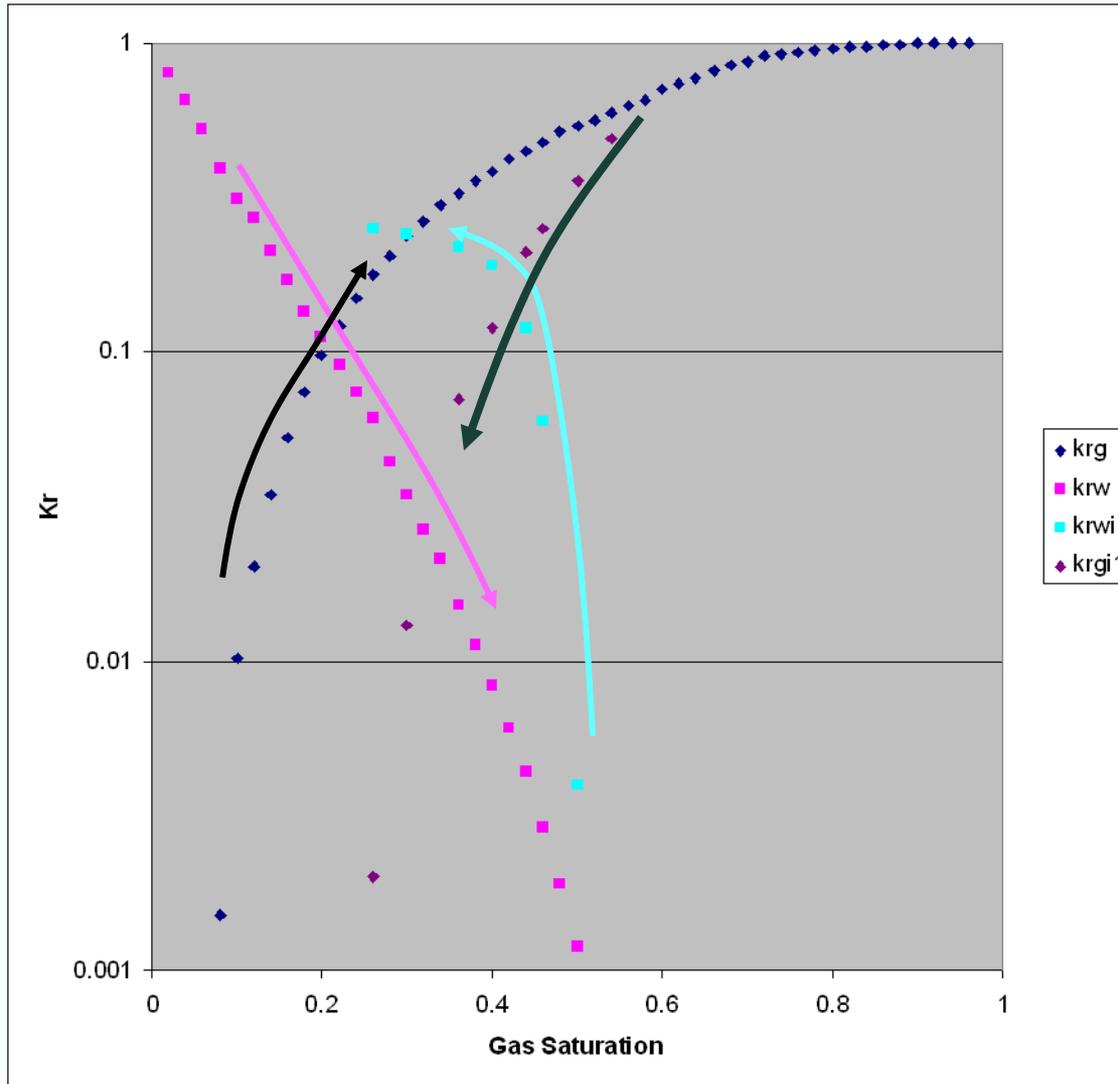




Pore Throats Blocked by Gas Force Flow Through Other Channels



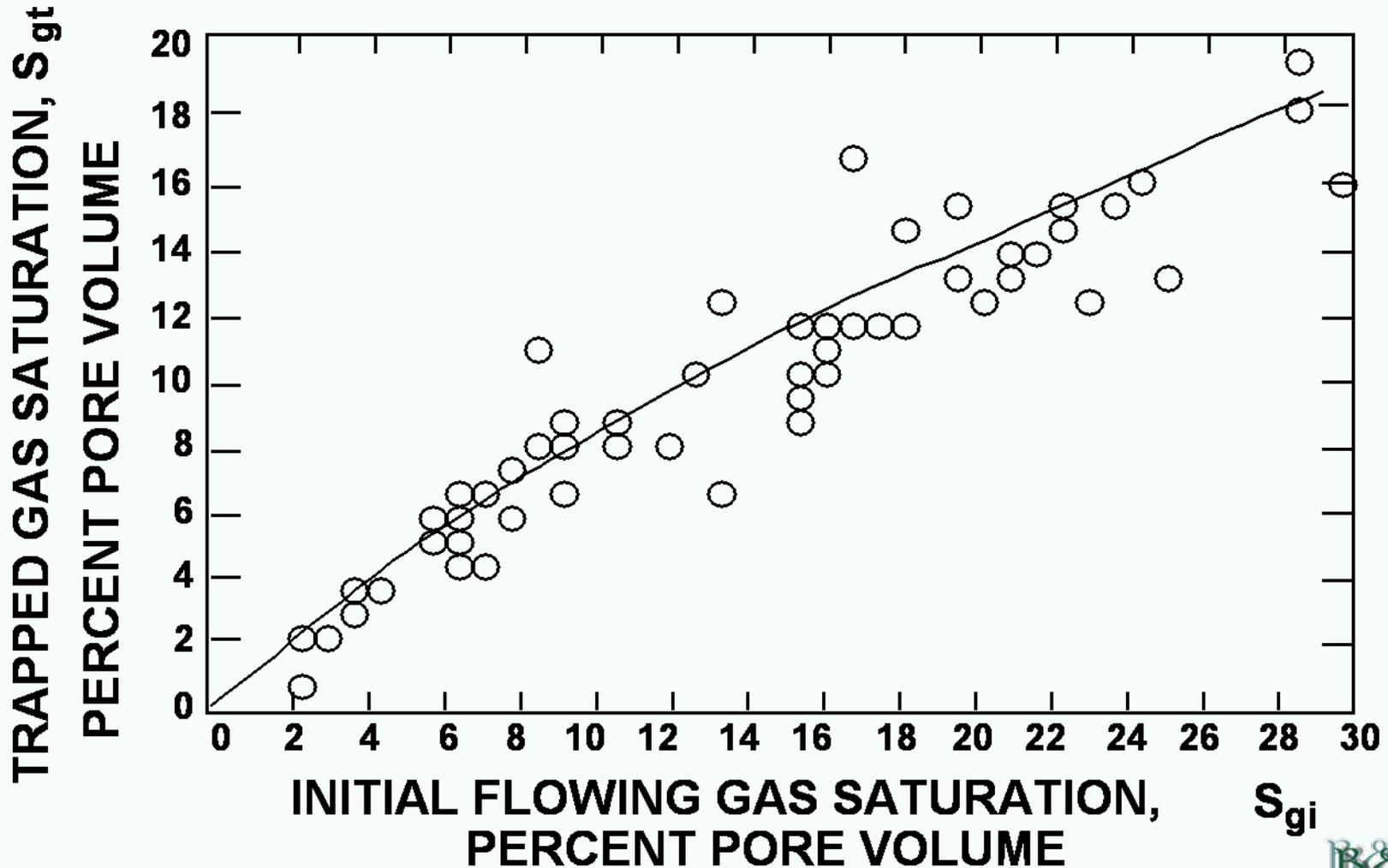
Gas-Water Rel-Perm Hysteresis



Hysteresis curves show effects of gas blockage and entry pressure.

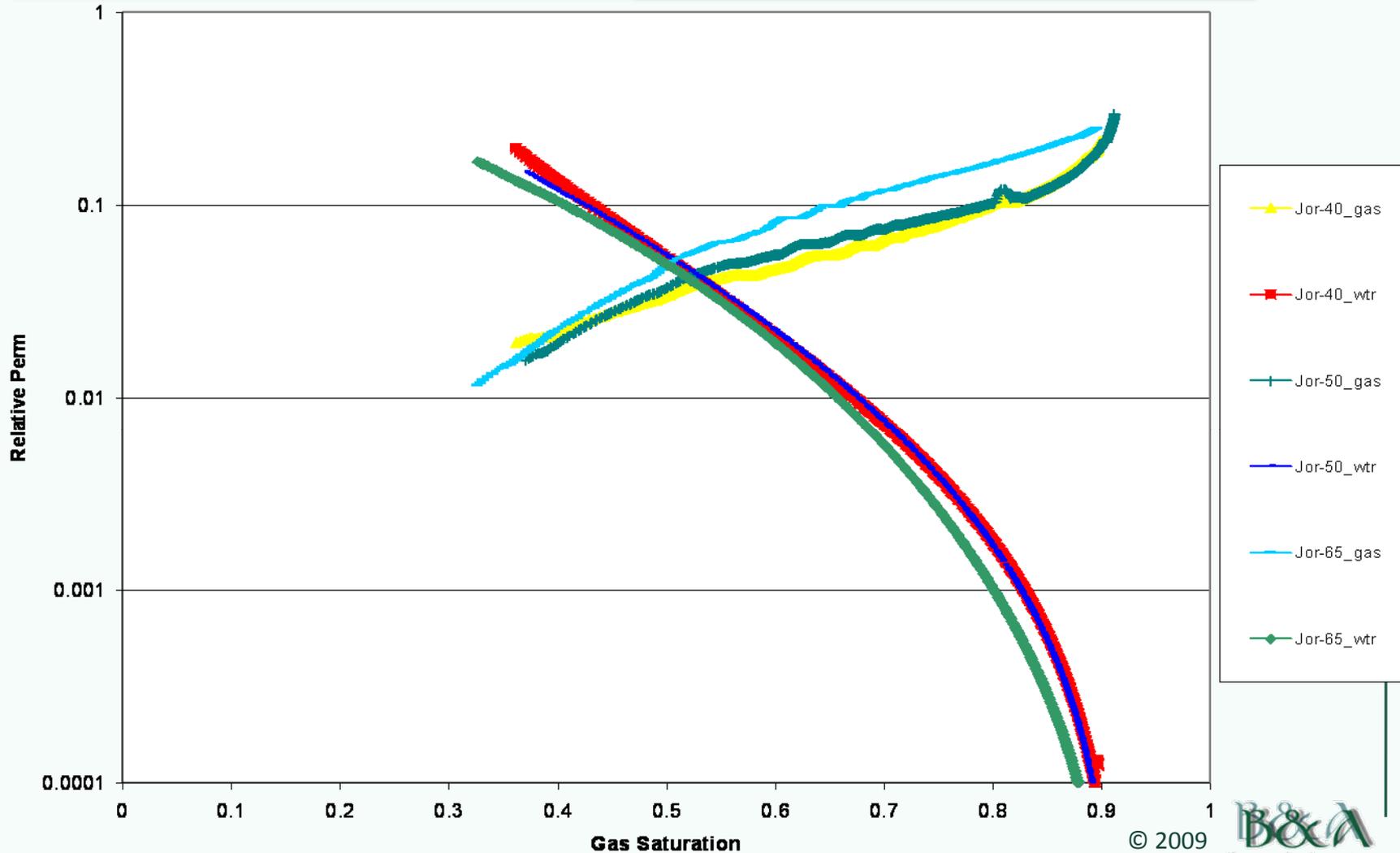
This can happen every time a well is killed or shut-in when liquid is injected or allowed to fall out in the tubing and imbibe.

Trapped Gas Increases with Initial Gas Saturation





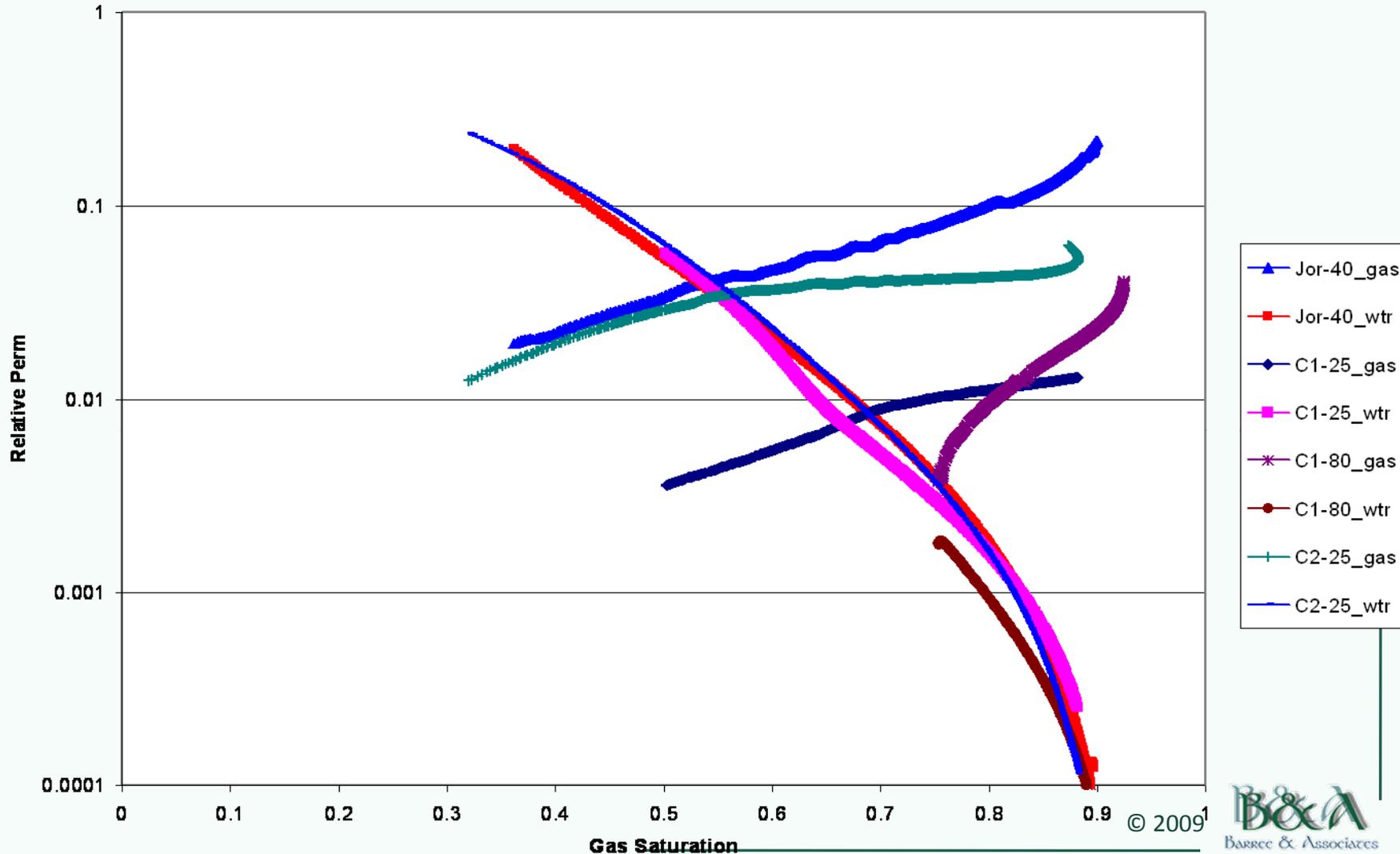
Summary of 16/30 Jordan Sand Data: Gas-Water Displacement Tests



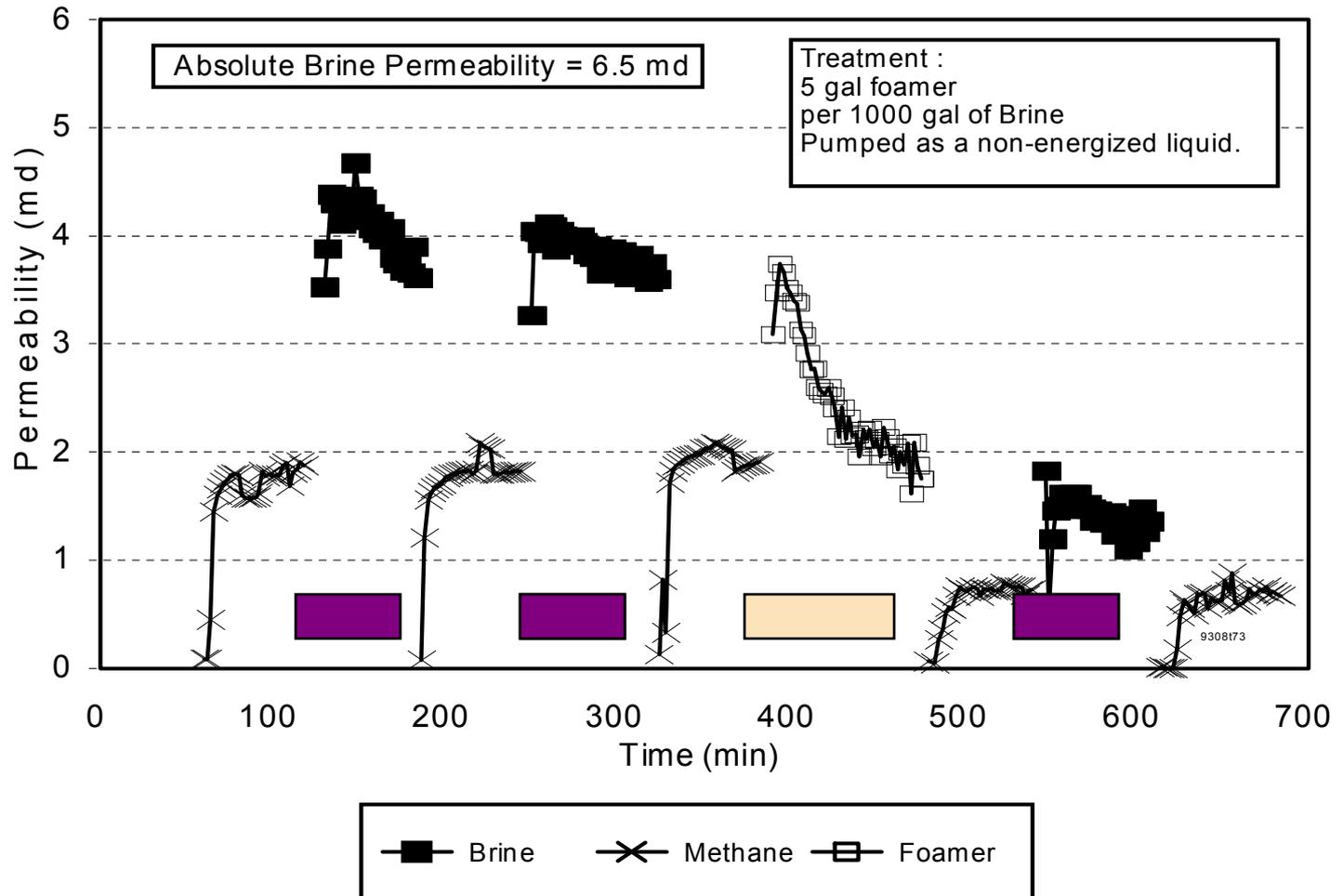
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Summary of Surfactant C Data with Saturation Offset Applied



Effects of Foamers on Gas Perm





Effect of Gas Blockage on Flowback

- Initial cleanup removes liquids and establishes gas permeability
- A shut-in or liquid-kill increases saturation around well and fracture face leading to trapped gas
- Permeability to all phases may be reduced significantly (and permanently)
- How a well is cleaned-up may as important as how it's frac'd
- Repeated well killing (for multi-zone fracs) is to be avoided
- Dewatering is a slow process but imbibition can be very fast

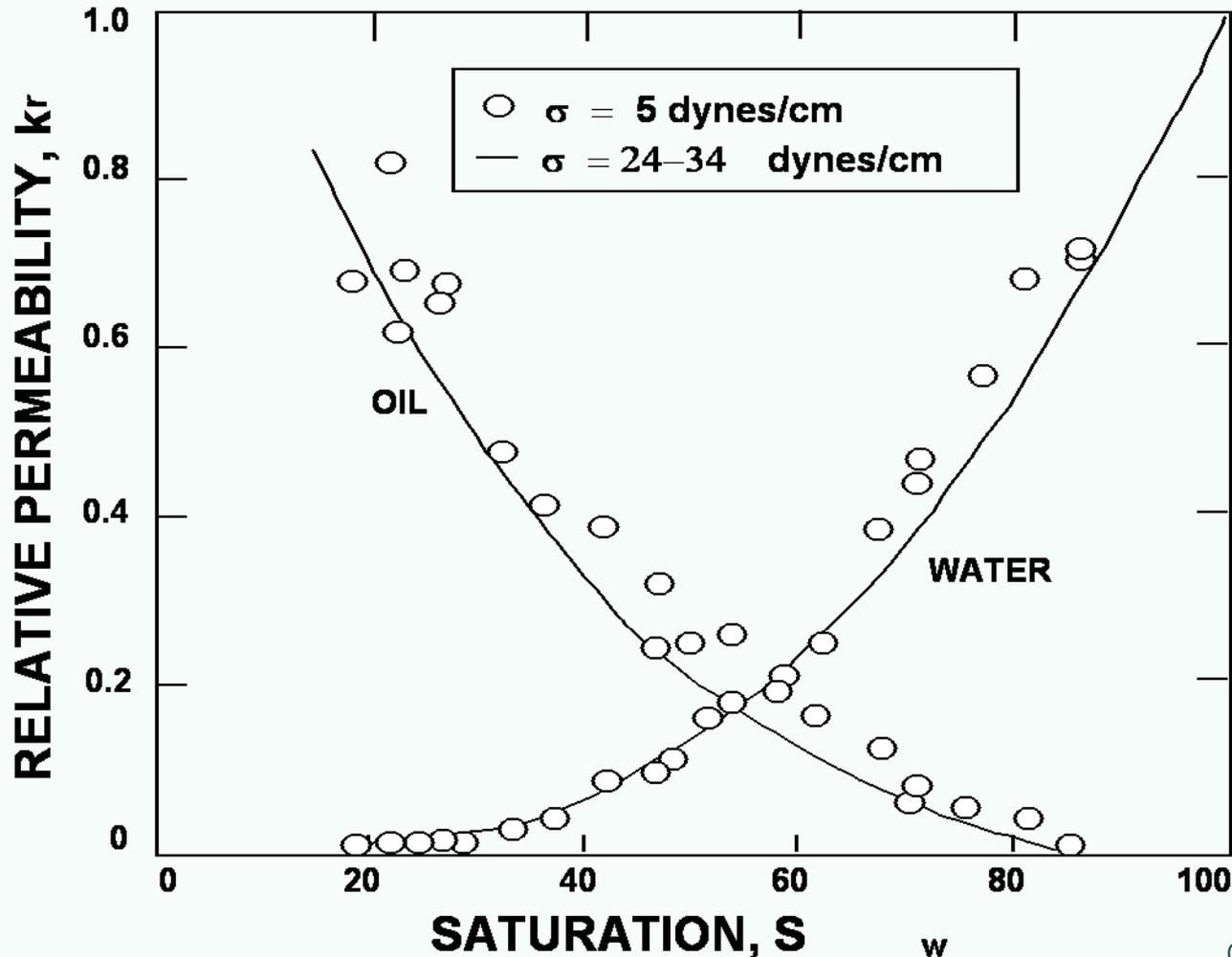


Correcting “Water Block”

- Use CO₂ or N₂ saturated fluids
- Try to lower interfacial tension (IFT) and capillary threshold pressure
- Change rel-perm curve through IFT reduction
- Add high-vapor pressure miscible fluid (MeOH) to system
- CO₂ “Huff-and-Puff” (for immobile water zones)
- Pump-off the well and maintain water level below perms until system “drains”



Moderate Changes in IFT Have Little Effect on Rel Perms



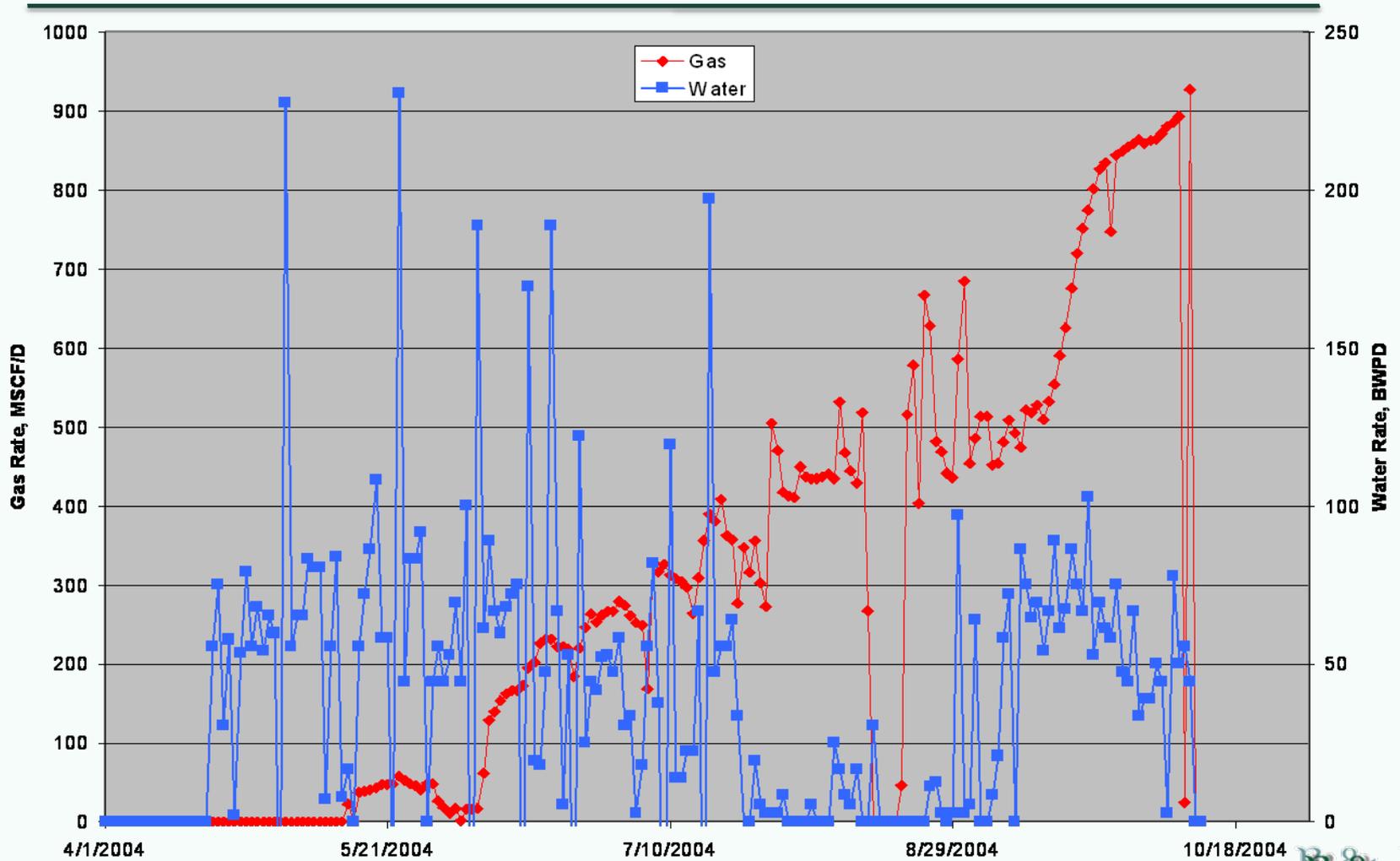


Example Well History: Recovering from Severe Water Loading

- Well “watered out” and died after losing fluid to the gas zone because of a casing leak
- Previous operator spent months gas lifting the well to unload water with no gas response
- Gas lifting proved unsuccessful and the well was given up for dead
- New operator purchased the well and installed a surplus pumping unit on April 14
- Well initially made 70 bwpd and no gas
- One month later the well showed signs of gas



Well Performance After Pump Installation





Results of Extended Rod-Pumping

- Almost 20,000 BW have been produced since the casing leak was repaired (about 8000 since
- Well continues to give up water with a current rate of about 48 bwpd
- Oil production rate has now increased to 5 bopd (about half of pre-leak rate)
- Gas rate has returned to pre-leak rate of about 1 MMSCF/D
- New operator has booked 100 MBOE additional reserves for this well



Clay Sensitivity and Control

- Different damage mechanisms require different treatment
 - Clay swelling
 - Clay hydration and extension
 - Fines migration and plugging
 - Cation exchange effects
 - Relative permeability damage

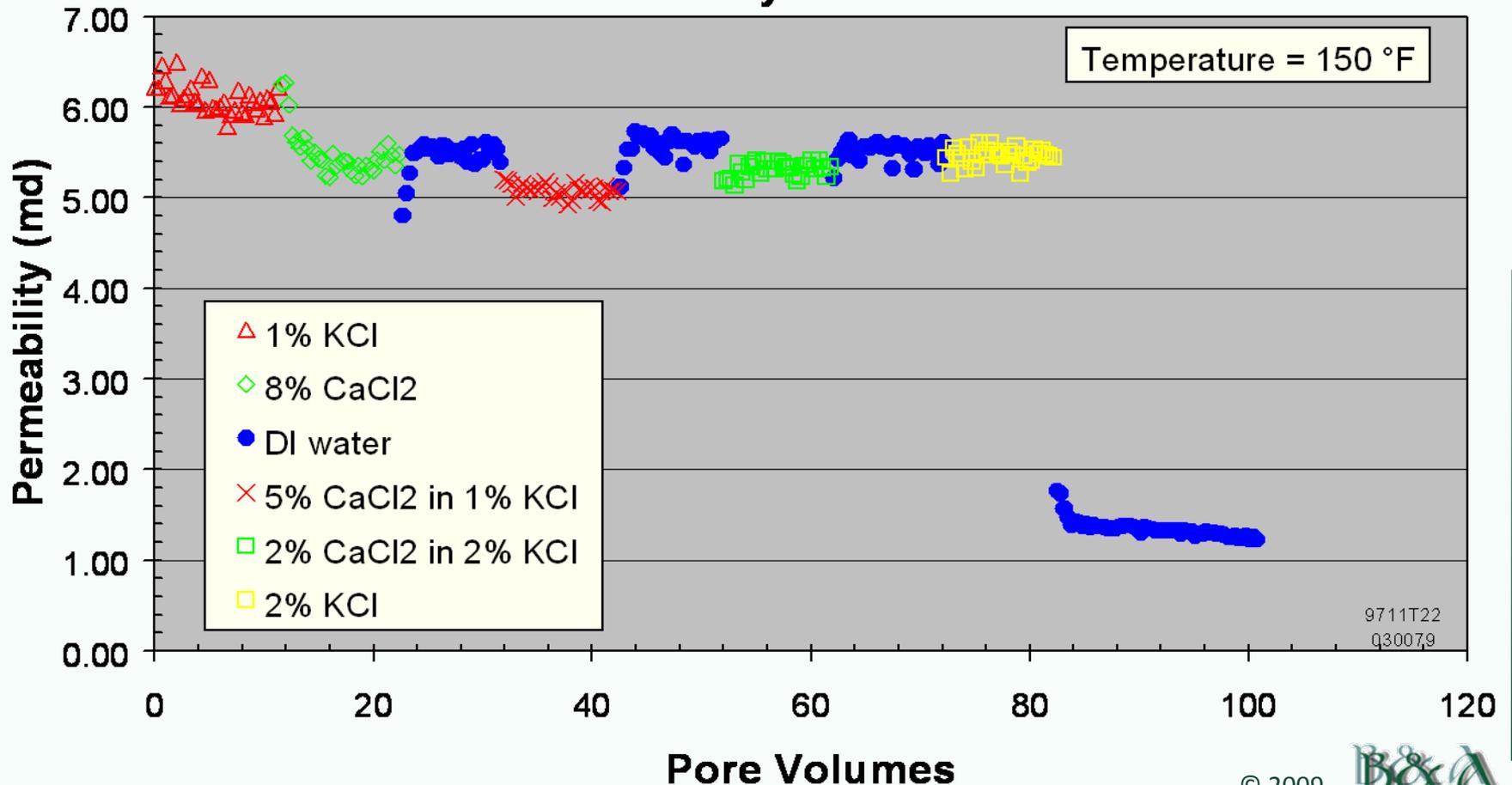


Formation Damage in Coal and Shale

- Identification of swelling and dispersing clays
 - Capillary suction time (CST)
 - Roller oven test
- Fluid-rock interactions and generation of fines
 - Effects of brine salinity and acid
 - Organic fluids can and will adsorb in coals
- Regained matrix permeability
 - Generally too low to measure with no damage
- Retained fracture conductivity
 - Stress effects
 - Fluid effects

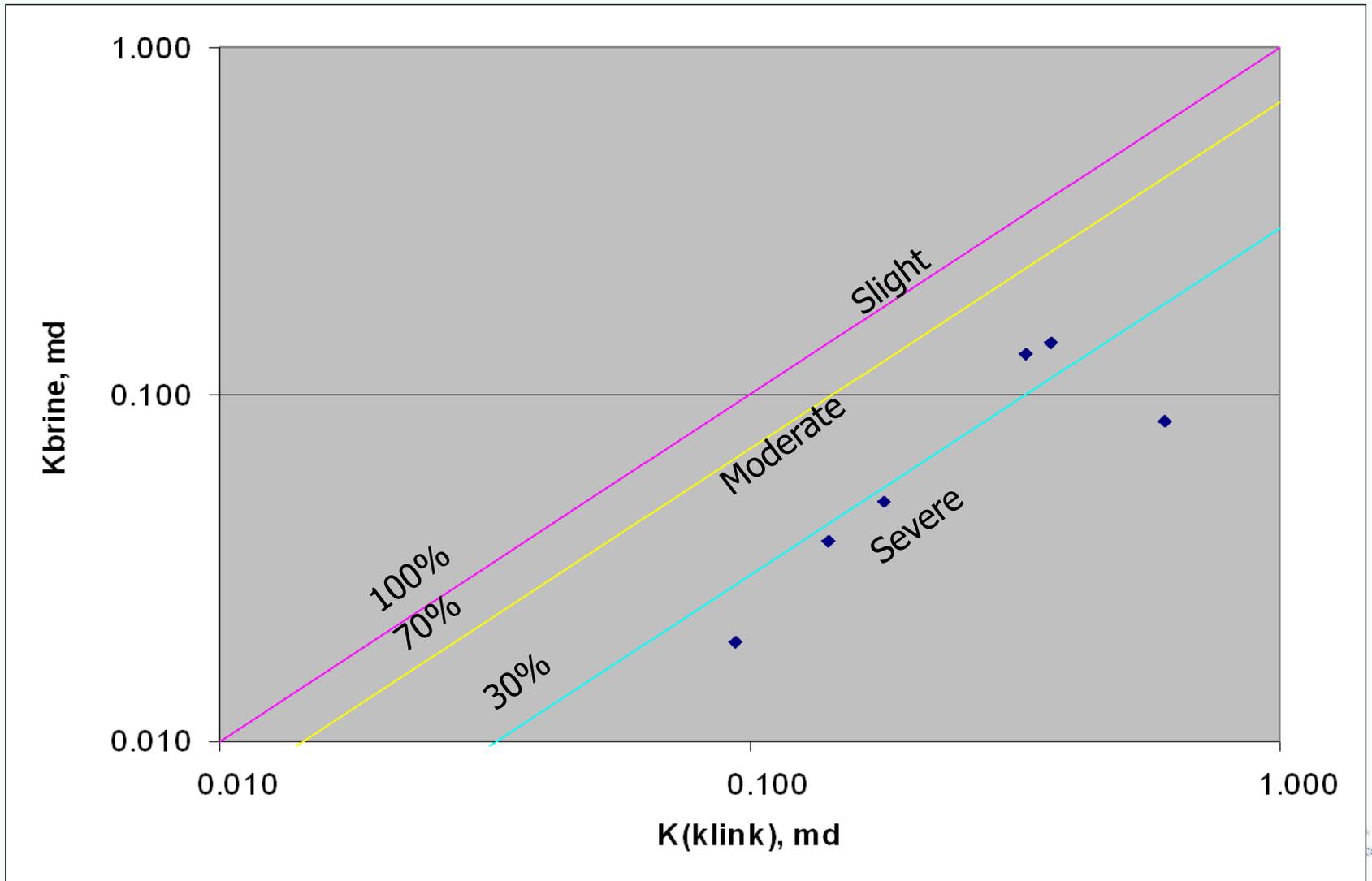
Bandera Sandstone: Effect of CaCl_2

Effect of Calcium Exchange to Potassium on the Relative Permeability of Bandera Sandstone





General Plot for Characterizing Water Sensitivity





Clay Effects on Permeability

- Will migrate
 - wrong cation, wrong salinity, wrong sequence
- Trap other migrating fines
 - degraded feldspars
- Other stabilizing mechanisms are present to prevent fresh water damage
 - Surface and interior cations
 - interior cations are very difficult to exchange
 - Other cations may be involved in “permanent” stability other than calcium



Recommendation

- Brine sensitivity can not be anticipated from core composition analysis alone.
- Other effects, most notably, relative permeability, may be the biggest problem
- Whole core or drilled sidewall cores are the answer:
 - location directed by logs
 - flow tests can confirm key factors
 - must know connate brine composition for most meaningful understanding.



Clay Control Additives and KCl Substitutes

- Polymeric additives for “nets” to lock migrating fines in place
- Ammonium salts enhance cation exchange and may liberate sodium or potassium
- Both are depleted by leading-edge contact and may only affect a limited reservoir volume
- Additives may work well “when they’re not needed”
- Base decisions on actual identified type of clay sensitivity



Where do we go from here?

- Improve geometry models
 - more and better fracture mapping data
 - collect and analyze more pressure data
 - conduct more post-frac tests
- Apply what we learn
 - continue to question models
 - allow models to expand to include
 - reservoir flow - falloff analysis - cleanup
 - wellbore effects - heat flow - chemistry



Where do we go?

- Improved job execution
 - cleaner fluids
 - better quality control
- Improve post-frac performance analysis
 - pressure buildups and multi-rate tests
 - production performance analysis
 - get and archive more data
 - make this a routine for all wells
 - polymer and water recovery analysis